			Tianjin <sub>.</sub>	All Best	Interna	tional Tr	ade Co.,	, Ltd					
(	DD	Wall Thickness		Unit	Weight		Steel Grade						
inch	mm		PPF (NU)	PPF (EU)	Kg/M	Kg/M	J55	K55	pipe end N80 L80 P1				
nen	11001			FFF(EU)		Kg/ M	100	1	100	100	P110		
		4.24	4		5.95		P/U	P/N	P/N	P/N	25.00		
		n († 1878) 1870 - State State († 1876)	12.115	4.7	6. 85	00000000000	V	V	V	V	V		
		4.83	4.6			6.99	P/N/U	P/N/U	P/N/U	P/N/U	P/N/U		
0.0/0	20.00	100 AP	2 2		0.00	0.05			V	V	V		
2 3/8	60.32	6.45	5.8	5.95	8.63	8.85			P/N/U	P/N/U	P/N/U		
		7.49	6.6		9.82					$\checkmark$			
		7.49	0.0		9.82					Р			
		8.53	7.35	7.45	10.94	11.09				$\checkmark$			
		0.00	1.00	1. 10	10. 54	11.09				P/U			
		5.51	6.4	6.5	9.52	9.67	V	$\checkmark$	V	V	V		
		5.51	0.4	0.0	5.52	5.01	P/N/U	P/N/U	P/N/U	P/N/U	P/N/U		
		7.01	7.8	7.9	11.61	11.76		_	$\checkmark$	V	V		
		1.01	1.0	1.0	11.01	11.10		-	P/N/U	P/N/U	P/N/U		
		7.82	8.6	8.7	12.8	12.95			V	N	V		
2 7/8	73.02					10.00			P/N/U	P/N/U	P/N/U		
7 0.817	0.0000000000000000000000000000000000000	8.64	9.35	9.45	13.91	14.06			10	N N			
				14 (4) (4) (5)	1 - 1 - 1		1	and the first set	10 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	P/U			
			10.5		15.63			2.0	10.00	N D			
				-	-	-	-			P √			
		11.18	11.5		17.11		1.1	20		P			

		0.45	9.2	9.3	13.69	10.04	$\checkmark$	$\checkmark$	$\checkmark$	V	$\checkmark$
		6.45	9.2	9, 3	13, 69	13.84	P/N/U	P/N/U	P/N/U	P/N/U	P/N/U
		7.34	10.2		15, 18		$\checkmark$	$\checkmark$	$\checkmark$	$\checkmark$	
		1.01	10, 2				P/N	P/N	P/N	P/N	
		9.52	12.7	12.95	18.9	19.27					V
		0.02	10.1	15,00	10, 0	10.01	-		-		P/N/U
3 1/2	88.9	10.92	14.3		21.28						
		12.09	15.5		23.07						
		13.46	17		25.3						
		5 10			11.46	5	$\checkmark$	V	$\checkmark$	V	
		5.49	7.7				P/U	P/N	P/N	P/N	$\checkmark$
		5.74	9.5		14.14		$\checkmark$	$\checkmark$	$\checkmark$	$\checkmark$	
4	101.16	5.74	9.0		14.14		P/N	P/N	P/N	P/N	P/N
4	101, 10	6.65	10.7	11		16.37	V	V	V	V	V
		0.00	10.1	3.1		10.01	P/U	P/U	P/U	P/U	P/U
4 1/2	114.3	6.88	12.6	12.75	18.75	18.97	V	V	V	V	V
A	111.0	0.00	1.000.00	10,10			P/N/U	P/N/U	P/N/U	P/N/U	P/N/U

					API 5CT	Steel Casii	ng Pipe								
	OD	thickness	Unit	Weight	Steel Grade										
inch	Imm	mm	PPF	Kg/M	J55	Thread Connection   5 K55 L80 N80 C90 T95 P110									
nen	inn	5. 21	9.5	14.14	√ P/STC	√ P/STC	100	100		150		Q125			
	114.3	5.69	10. 5	15.63	√ P/STC/BTC	P/STC/BTC		1			5 25				
4 1/2		6.35	11.6	17.26	P/S/L/B	P/S/L/B	√ P/L/B	√ P/L/B	√ P/L/B	√ P/L/B	√ P/L/B				
		7.37	13. 5	20.09		1/0/1/0	$\sqrt{\frac{P/L}{B}}$	$\sqrt{\frac{P/L}{B}}$	√ P/L/B	V P/L/B	$\sqrt{P/L/B}$	6			
		8.56	15.1	22.47			1,0,0				$\sqrt{P/L/B}$	√ P/L/B			
		5. 59	11. 5	17.11	√ P/S	√ P/S									
		6. 43	13. 5	19.35	√ P/S/L/B	√ P/S/L/B									
		7.52	15	22.32	√ P/S/L/B/E	$\sqrt{\frac{P/S/L/B/E}{}}$	√ P/L/B/E	√ P/L/B/E	√ P/L/B/E	√ P/L/B/E	√ P/L/B/E	5 5			
5	127	9.19	18	26. 79			√ P/L/B/E	√ P/L/B/E	√ P/L/B/E	√ P/L/B/E	√ P/L/B/E	√ P/L/B/I			
		11.1	21.4	31.85			$\sqrt{P/L/B}$	$\sqrt{\frac{1}{P/L/B}}$	√ P/L/B	√ P/L/B	√ P/L/B	√ P/L/B			
		12.14	23. 2	34. 53				$\sqrt{\frac{1}{P/L/B}}$	V	√ P/L/B	$\sqrt{P/L/B}$	√ P/L/B			
		12.7	24.1	35.86				P/L/B P/L/B	P/L/B $\sqrt{P/L/B}$	P/L/B √ P/L/B	P/L/B $\sqrt{P/L/B}$	$\frac{P/L/B}{V}$			

Г

		85000	17207	100000000000	V	V		1	1			
		6.2	14	20.83	P/S	P/S						1
	1 1	C 00	15.5	00.07	V	V						1
		6.98	15. 5	23.07	P/S/L/B/E	P/S/L/B/E						
$5 \ 1/2$	139.7	7.72	17	25.3	N	V	V	V	N	V	N	3
5 1/2	159.7	1.72	11	20. 5	P/S/L/B/E	P/S/L/B/E	P/L/B/E	P/L/B/E	P/L/B/E	P/L/B/E	P/L/B/E	
		9.17	20	29.76			V	V	V	V	V	
		5.11	40	45.10			P/L/B/E	P/L/B/E	P/L/B/E	P/L/B/E	P/L/B/E	
		10.54	23	34.23			V	V	V	V	N	V
		10.01	20	01.20			P/L/B/E	P/L/B/E	P/L/B/E	P/L/B/E	P/L/B/E	P/L/B/E
		7.32	20	29.76	V	V		-	-	-		
					P/S/L/B	P/S/L/B	1	1	1		1	
		8.94	24	35.72	N	N	N.	N In the test	N In the last	N In the test	N	-
6 5/8	168.28	CREATE .	105.00	200000-30001 200000-30001	P/S/L/B/E	P/S/L/B/E	P/L/B/E	P/L/B/E	P/L/B/E	P/L/B/E	P/L/B/E	
	10.00000000000	10.59	28	41.67			N ID ID	N (D (D)	N ID ID	N In /n /n	N ID / D / D	
			-				P/L/B/E	P/L/B/E	P/L/B/E	P/L/B/E	P/L/B/E	CT
		12.06 33	32	47.62			N D /L /D /D	N D/L/D/D	N D/L/D/D	N D /L /D /D	γ D /L /D /D	N D/L/D/D
			1		1	V	P/L/B/E	P/L/B/E	P/L/B/E	P/L/B/E	P/L/B/E	P/L/B/E
		6.91	20	29.76	v P/S	P/S		-	-			
		8.05	23	34.23	F/5	P/5	N	1	1	1		2
					P/S/L/B/E	P/S/L/B/E	P/L/B/E	P/L/B/E	P/L/B/E	P/L/B/E		
				820000000	V	V V D/L	V D/D/D	N D/L	V D/D/D	V D/L	N	
		9.19	26	38, 69	P/S/L/B/E	P/S/L/B/E	P/L/B/E	P/L/B/E	P/L/B/E	P/L/B/E	P/L/B/E	
	1				1/0/0/0/0	170/1/0/1	V	√ √	V	V	V	1
7	177.8	10.36	29	43.16			P/L/B/E	P/L/B/E	P/L/B/E	P/L/B/E	P/L/B/E	
	1 1	035235		020030		8	V	V	V	V	V	2
		11.51	32	47.62			P/L/B/E	P/L/B/E	P/L/B/E	P/L/B/E	P/L/B/E	
		2 XT-802704283.5	0.02223	02200230			V	V	V	V	V	V
		12.65	35	52.09			P/L/B/E	P/L/B/E	P/L/B/E	P/L/B/E	P/L/B/E	P/L/B/E
		10 20		CEO EE			V	$\checkmark$	V	V	V	V
		13.72	38	56.55			P/L/B/E	P/L/B/E	P/L/B/E	P/L/B/E	P/L/B/E	P/L/B/E

		0.00	00.4	20.00	V	V	V	$\checkmark$	N	V	V	
		8, 33	26.4	39, 29	P/S/L/B/E	P/S/L/B/E	P/L/B/E	P/L/B/E	P/L/B/E	P/L/B/E	P/L/B/E	
		0.50	00.7	22.0			$\checkmark$	$\checkmark$	$\checkmark$	$\checkmark$	$\checkmark$	
		9.52	29.7	44.2			P/L/B/E	P/L/B/E	P/L/B/E	P/L/B/E	P/L/B/E	
		10.92	33.7	50.15			$\checkmark$	$\checkmark$	N	$\checkmark$	$\checkmark$	- 2
		10. 92	33.1	50.15			P/L/B/E	P/L/B/E	P/L/B/E	P/L/B/E	P/L/B/E	
	193.68	12.7	39	58.04			$\checkmark$	$\checkmark$	$\checkmark$	V	$\checkmark$	$\checkmark$
		14.1		56.04			P/L/B/E	P/L/B/E	P/L/B/E	P/L/B/E	P/L/B/E	P/L/B/E
7 5/8		14.27	42.8	63.69			$\checkmark$	V	V	V		V
1 0/0	195.00	14.27	42.0	03.09			P/L/B	P/L/B	P/L/B	P/L/B	P/L/B	P/L/B
		15.11	45.3	67.41	15		V	$\checkmark$	$\checkmark$	V	V	$\checkmark$
		10.11	40.0	01, 41			P/L/B	P/L/B	P/L/B	P/L/B	P/L/B	P/L/B
		15.88	47.1	70.09			V	V	V	V	V	V
		13.00	47.1	10.05			P/L/B	P/L/B	P/L/B	P/L/B	P/L/B	P/L/B
		17.45	51.2	76.19					N	V		
	-	17.40	11.10 01.2					1	Р	Р		
		19.05	55.3	82.3					V	V		2
		15.05	00.0	02.0				10	Р	Р		2
7 3/4	196.85	15.11	46.1	46.1 68.6					N	V		
1 0/ 1	1.00.00	10.11	10.1	00.0			-		Р	Р		
		8.94	32	47.62	V	V				-		6
		0.01	04	- 41.02	P/S/L/B/E	P/S/L/B/E		1			1	13
		10.16	36	53. 57	N	V	V	N	N	V	V	
		10,10	00	00101	P/S/L/B/E	P/S/L/B/E	P/L/B/E	P/L/B/E	P/L/B/E	P/L/B/E	P/L/B/E	
8 5/8	219.08	11.43	40	59.53			N	V	N	V	N	13
0 07.0		11.10	11.45 40	00.00			P/L/B/E	P/L/B/E	P/L/B/E	P/L/B/E	P/L/B/E	
		12.7	44	65, 48	-		V	N	N	V	N	
			0.15	10000000	-		P/L/B/E	P/L/B/E	P/L/B/E	P/L/B/E	P/L/B/E	2
		14.15	49	72.92	-		N	N	N	V	N	3
		*****	1.0440				P/L/B/E	P/L/B/E	P/L/B/E	P/L/B/E	P/L/B/E	

		8.94	36	53. 57	√ P/S/L/B/E	√ P/S/L/B/E		-			
		10.03	40	59.53	V	V	V	V	V	V	
	244. 48	10.05	UL.	33, 30	P/S/L/B/E	P/S/L/B/E	P/L/B/E	P/L/B/E	P/L/B/E	P/L/B/E	1
		11.05	43, 5	64.73			P/L/B/E	P/L/B/E	P/L/B/E	P/L/B/E	P/L/B/E
9 5/8		11.99	47	69.94		-	√ P/L/B/E	√ P/L/B/E	√ P/L/B/E	√ P/L/B/E	√ P/L/B/E
		13.84	53. 5	79.62			V	$\checkmark$	V	V	V
		15, 11	58.4	86.91			P/L/B/E √	P/L/B/E √	P/L/B/E √	P/L/B/E √	P/L/B/E √
		10, 11	00.1	00.01	1	1	P/L/B	P/L/B	P/L/B	P/L/B	P/L/B
	273. 05	8.89	40.5	60.27	P/S/B	N P/S/B		8			
		10.16	45. 5	67.71	√ P/S/B/E	√ P/S/B/E		ili N			
				75.9	√ √	V	1	1	V	V	1
		11.43	51		P/S/B/E	P/S/B/E	P/S/B/E	P/S/B/E	P/S/B/E	P/S/B/E	P/S/B/E
10 3/4		12.57	55.5	82, 59			V D/C/D/D	V D/C/D/D	V	V	V D (C (D (D
	+	- 60029400420		-	-	P/S/B/E	P/S/B/E	P/S/B/E	P/S/B/E	P/S/B/E	
		13.84	60.7	90.33		Î			P/S/B/E	P/S/B/E	P/S/B/E
		15.11	65.7	97.77				2	V	V	V
		101 11			210	1		2	P/S/B	P/S/B	P/S/B
		9.53	47	69.94	N P/S/B	N P/S/B	2		-		
					V	V	1				
11 3/4	298.45	11.05	54	80, 36	P/S/B	P/S/B	<u>[</u>				
		12.42	60	89.29	V	V		2			
		10.10		00100	P/S/B	P/S/B					

		9.65	54.5	81.1	N	N						
		9.00	54.5	01.1	P/S/B	P/S/B					Û.	1
		10.00	61	00.50	$\checkmark$	$\checkmark$						0
12 2/0	220 70	10.92	01	90.78	P/S/B	P/S/B				-2		
13 3/8	339.72	10 10	00	101 10	N	V	$\checkmark$	V	N	V	$\checkmark$	
		12.19	68	101.19	P/S/B	P/S/B	P/S/B	P/S/B	P/S/B	P/S/B	P/S/B	l.
	1	12 06	70	107 15			$\checkmark$	V	V	V	V	$\checkmark$
		13.06	72	107.15			P/S/B	P/S/B	P/S/B	P/S/B	P/S/B	P/S/B
		11 19	75	111.61	$\checkmark$	V						
		11.13			P/S/B	P/S/B						
16	406.4	12.57	84	125.01	$\checkmark$	V				- 2		
	400.4	12.57			P/S/B	P/S/B		10		2	1	2
		16.66	100	162.21	$\checkmark$	V	V	$\checkmark$	$\checkmark$	V	V	V
			109		Р	Р	Р	Р	Р	Р	Р	Р
18 5/8	479.00	08 11.05	5 87.5	130. 21	$\checkmark$	V						
18 9/8	473.08				P/S/B	P/S/B						
		11 12	94	120 00	$\checkmark$	V						j.
		11.13	94	139.89	P/S/L/B	P/S/L/B						
20	508	12.7	106.5	158.49	$\checkmark$	V						
20	506	12.7	100. 5	106.49	P/S/L/B	P/S/L/B						1
		10.10	199	107 02	$\checkmark$	V						
		10, 15	135	191.95	P/S/L/B	P/S/L/B	2	-				3
		16.13	133 Note:	197. 93 I	P/S/L/B P=Plain En	a <sup>C</sup> recreases to	S=BTC L=L'	TC E=Extr	eme line			

Tianjin All Best International Trade Co., Ltd is a famous provider of steel pipe fittings.

Our business involves Oil & Gas Industry, Mining Industry, Automobile Industry, Chemical Industry and Construction Industry.

Our products include elbow, flange, reducer, pipe cap, tee and corrugated expansion joint and seamless steel line pipe. We have got g ood recognition from our customers in South America, South East Asia and North Africa.

These pipe fittings can be made according to both GB and International standards, ASME, DIN, BS, JIS & GOST. In the last years, we g ot API 5L, and API Q1 international certification for the products. ISO9001, ISO14001, and OHAS18001 are three basic certificate for our q uality, service, environment and workers' qualification.

Our factory covers an area of 70000 square meters in Xiwang New District, Mengcun County, Cangzhou, Hebei, China. With advanced equipment, excellent management, skilled workers, and ambitious salesmen, we have great confidence to provide you with better products w ith the most reasonable price. To win customers's belief in us is the goal for the whole company for ever.

Welcome you to visit us in China or send emails to us. We love friends and like the reply buttons.

Contact us

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